

# Procemin-GEOMET 2018

14<sup>th</sup> International Mineral Processing Conference  
5<sup>th</sup> International Seminar on Geometallurgy

## New Predictive Blasting Model Oriented to Optimum Production Planning

Jorge M. Menacho, L.A Verdugo and G.E. Vega, [drm@drm.cl](mailto:drm@drm.cl)  
De Re Metallica Ingenieria, DRM Technology SpA

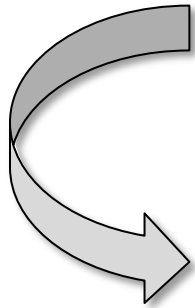
# Introduction



## Blasting Objectives

- (i) Maximizing the SAG mill throughput by providing it with the optimum feed size distribution
- (ii) Optimizing the blast fragmentation and muckpile profile to maximize the productivity of load and haul operations
- (iii) Minimizing orebody dilution and high wall damage due to blasting
- (iv) Minimizing the operation cost of the whole production chain.

# Introduction



## Main Models

- (i) Kuz-Ram
- (ii) JKRCM (CZM, TCM)
- (iii) Swebrec

Model	Type
Kuz-Ram	Empirical, 3 basic equations
JKMRC: "The Crushed Zone Model"	Empirical, bimodal Kuz-Ram type
JKMRC: "The Two Component Model"	Empirical, bimodal Kuz-Ram type
Ouchterlony (Swebrec function)	Empirical, bimodal

# Phenomenological Approach

## Mineral Variables:

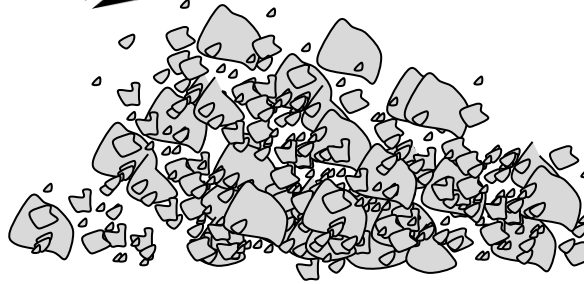
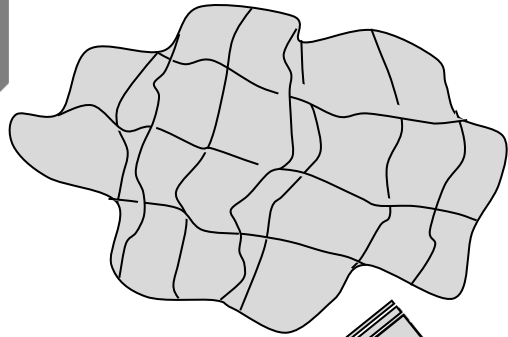
Tonnage  
Blast area  
Physical Quality

## Process Variables:

Powder factor  
Burden and spacing  
Drilling diameter  
Type of blast  
Initiator  
Multiple blast

## Internal Variables per Quality:

Fragmentation habit  
Specific rate of fragmentation



## Responses:

ROM size profile  
Energy consumption

# Population Balance

$$\frac{dw_i(\bar{E})}{d\bar{E}} = -S_i^E w_i(\bar{E}) + \sum_{\substack{j=1 \\ i>1}}^{i-1} b_{ij} S_j^E w_j(\bar{E})$$

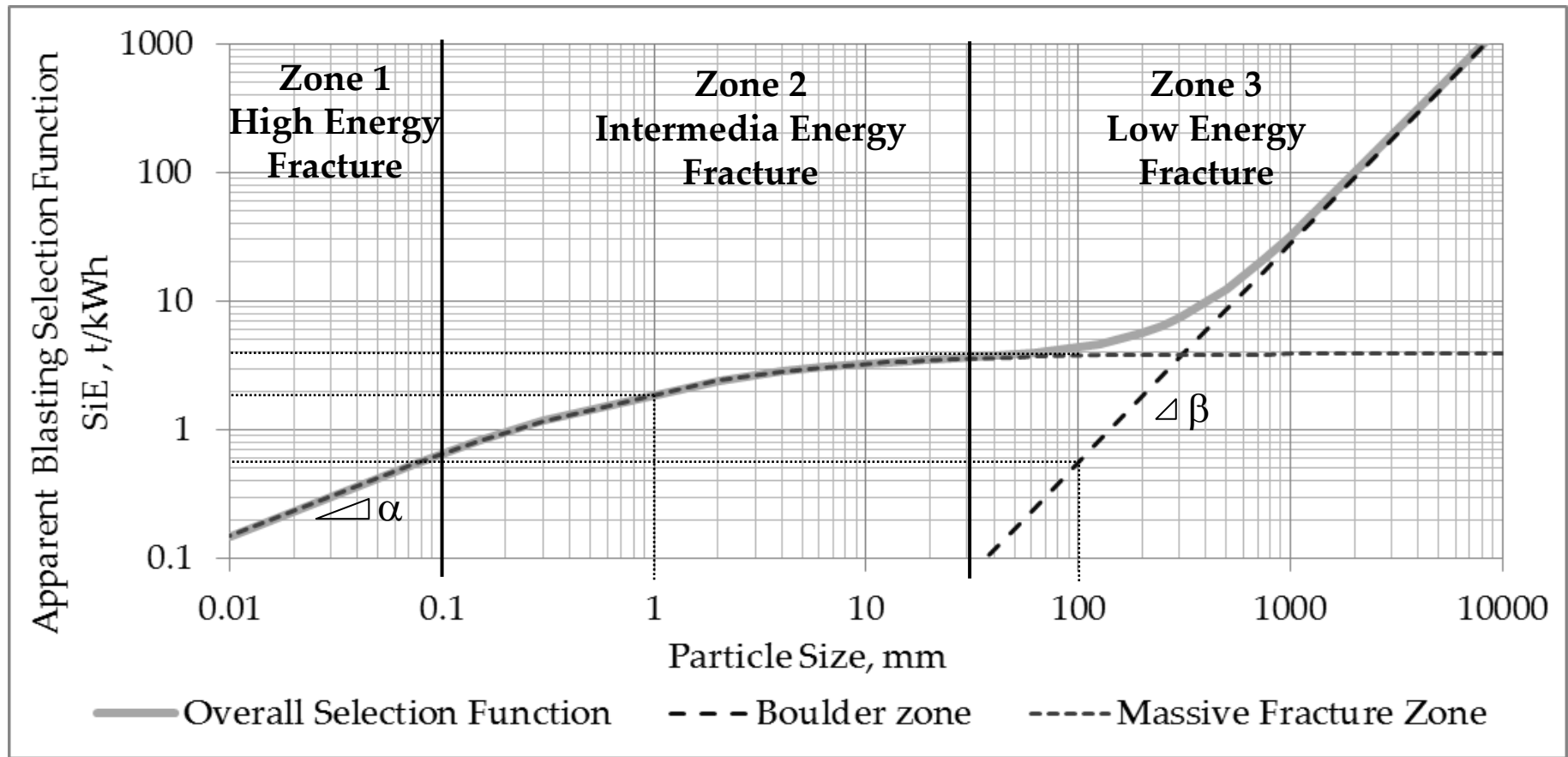
$$w_i(\bar{E}) = \sum_{j=1}^i a_{ij} e^{-S_j^E \bar{E}}$$

$$a_{ij} = \begin{cases} 0 & i < j \\ w_i(0) - \sum_{\substack{k=1 \\ i>1}}^{i-1} a_{ik} & i = j \\ \frac{1}{S_i^E - S_j^E} \sum_{k=j}^{i-1} S_k^E b_{ik} a_{kj} & i > j \end{cases}$$

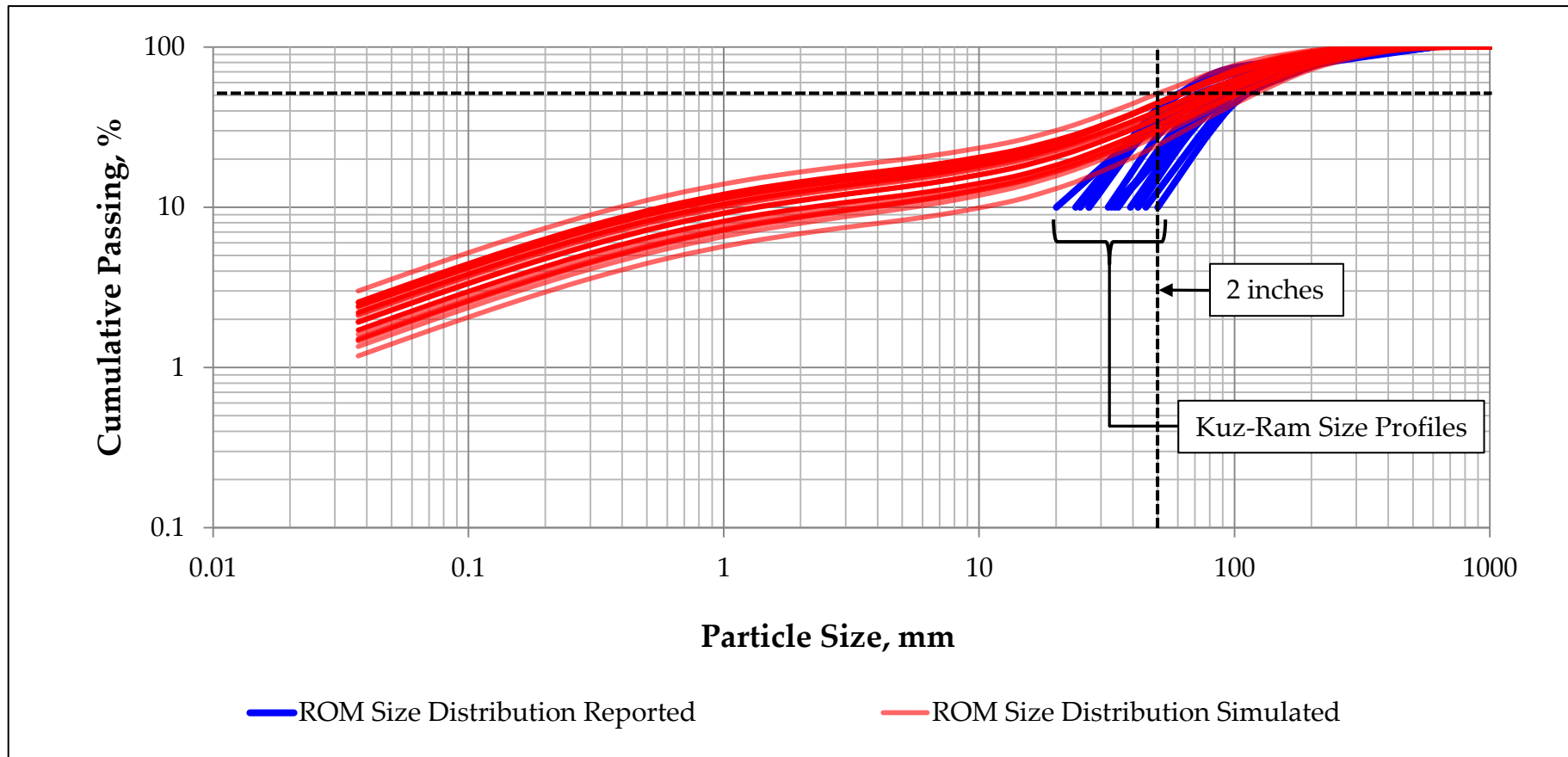
$$\frac{dR_i(\bar{E})}{d\bar{E}} = \sum_{\substack{j=1 \\ i>1}}^{i-1} B_{ij} S_j^E w_j(\bar{E}); \quad B_{ij} S_j \simeq S_i \Rightarrow P_i = 1 - \sum_k f_k (1 - F_i) \exp\left(-S_{ik}^E \bar{E}\right)$$

$$S_{ik}^E = \prod_i \left( \frac{p_i}{p_{i \text{ Ref}}} \right)^{\varepsilon p_i} \left\{ a_k \left( \frac{x_i}{x_0} \right)^{\alpha_{1k}} \left( \frac{1}{1 + \left( \frac{x_i}{x_0} \right)^{\alpha_{1k}}} \right) + b_k \left( \frac{x_i}{x_1} \right)^{\beta_k} \right\}; \quad \bar{E} = FC \times P_e$$

# The Selection Function: Scale Up Criteria



# Typical ROM Particle Size Profile

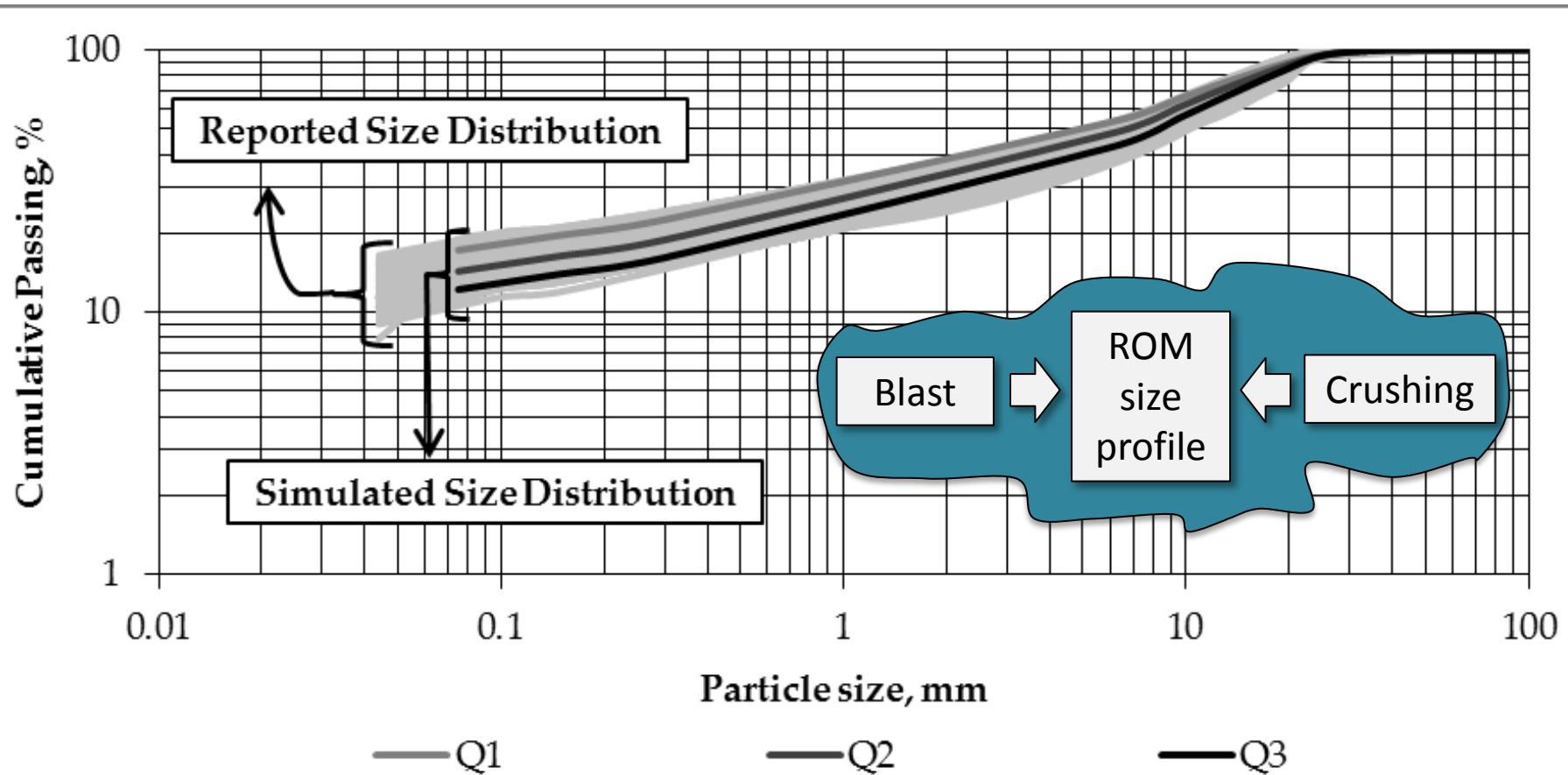


# Applications

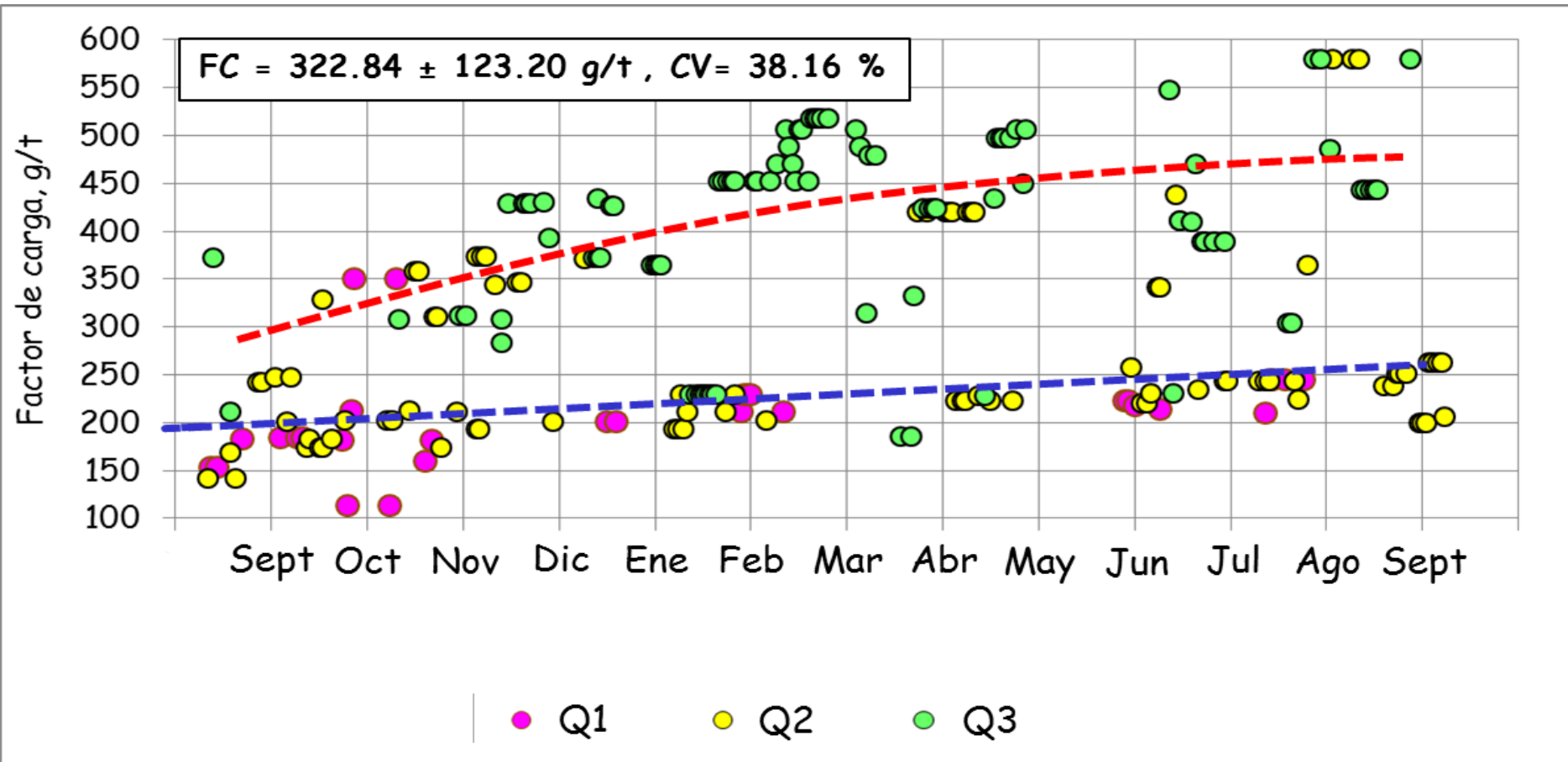
This blast simulation model has been successfully applied at CODELCO DGM, AMSA Antucoya, BHP Spence and CODELCO DRT, either for diagnosis, optimization or production planning purposes



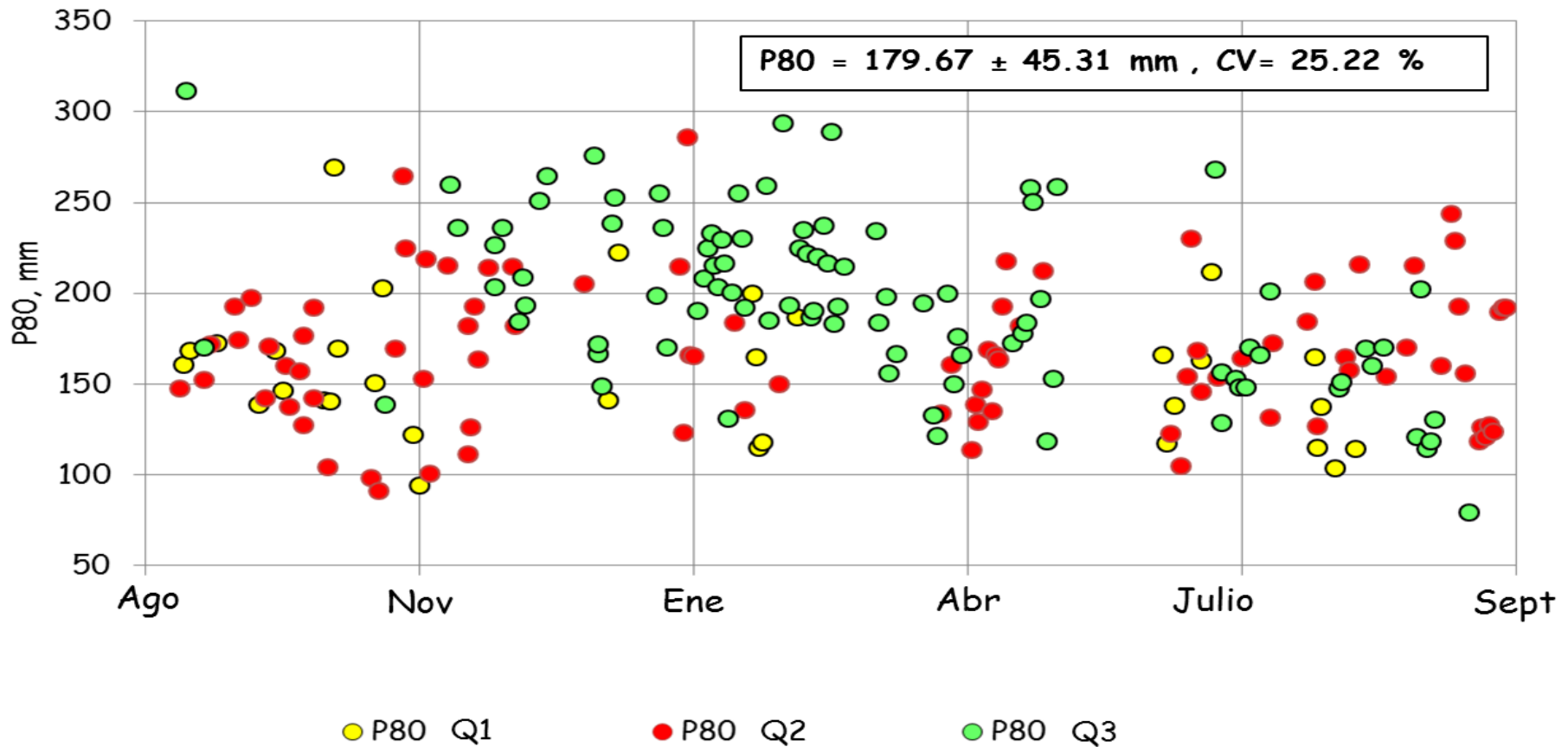
# Inverse Simulation: Mine-Plant Matching



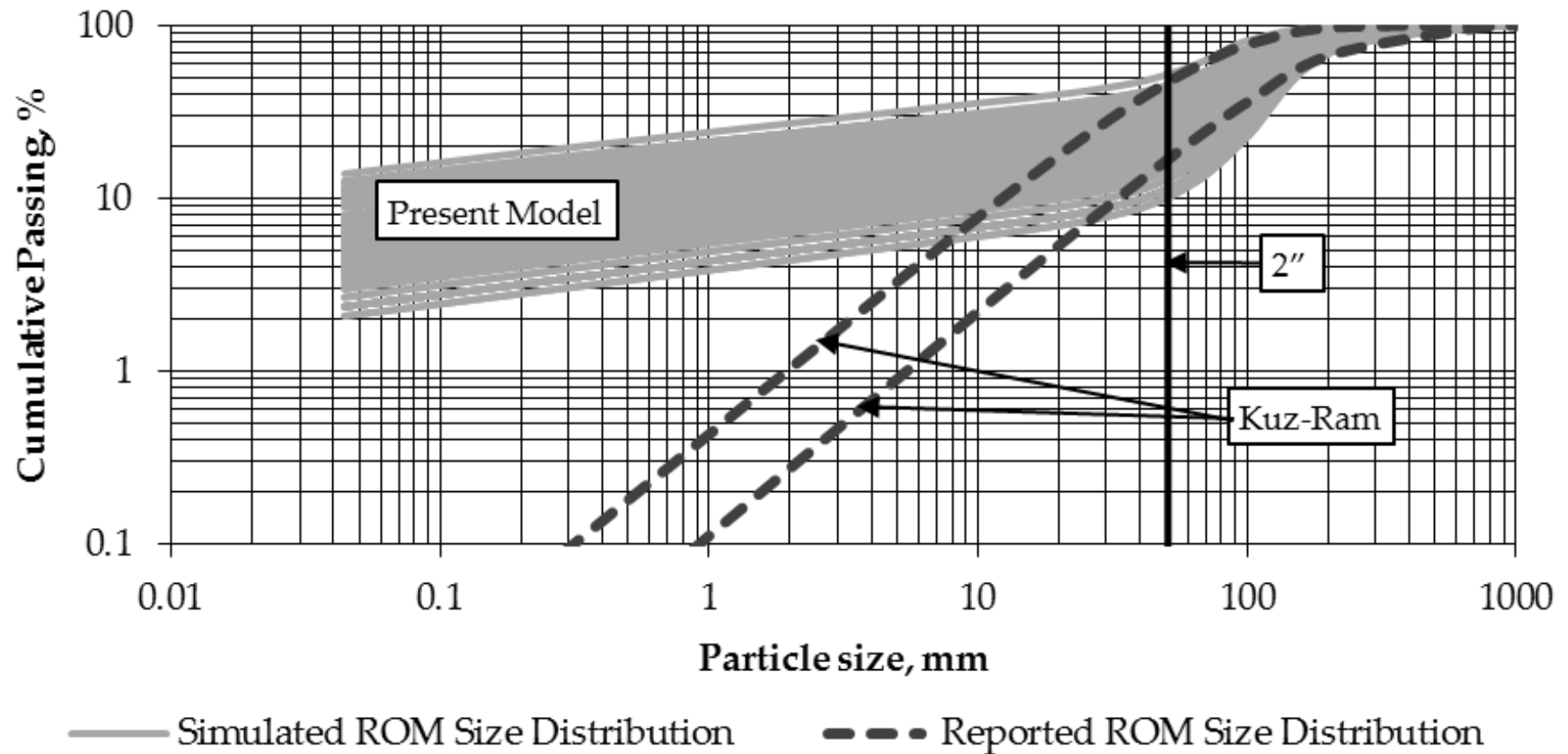
# Blasting Auditing



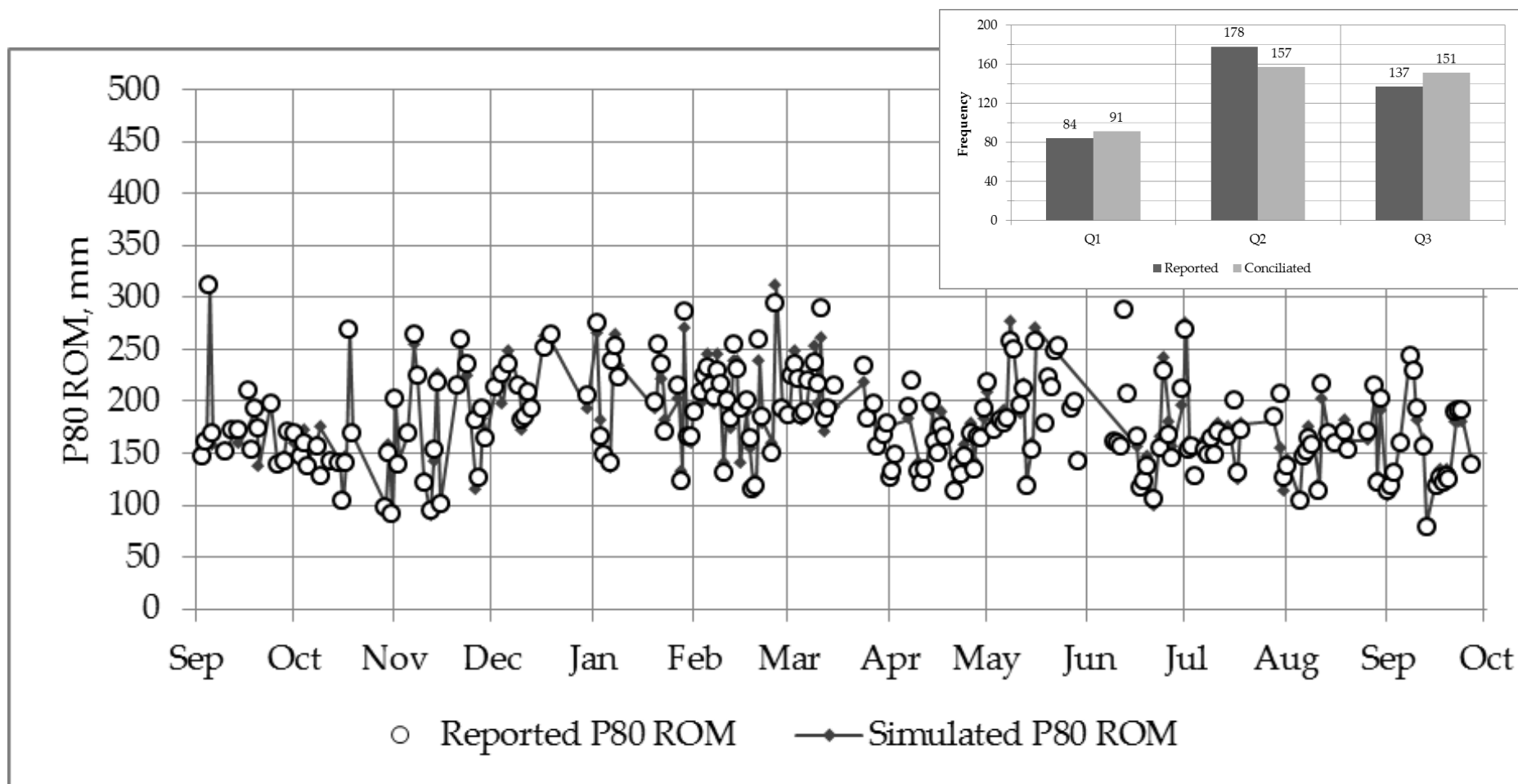
# Blasting Auditing



# Forecasting the Fines



# Physical Quality Conciliation



# Conclusions

A new phenomenological model to predict size distribution of blasted ores has been developed with clear advantages over the state of the art. It can be used for diagnosis, optimization and especially production planning issues.

Fragmented rocks in blasting usually follow a bimodal profile in log-log scale fairly well predicted by the present model.

Bimodal size distributions are attributed to a dual fragmentation mechanism. One driving to incomplete fracture of the coarse rocks and the other producing fines following a characteristic breakage pattern with root in the fractal genesis of the orebody.

The fines profile is correctly predicted by the phenomenological model. It drives to more fines compared to those estimated by the empirical standard models. A back-calculation procedure at the crushing and grinding plant supports the validity of the blast size-model estimations.

Finally, a method to forecast blasted muck size profiles is outlined.